

# APPLICATION OF THE SEMI-CLASSICAL FERMION $\mu$ -SPACE DENSITY TO NUCLEI USING WOODS-SAXON POTENTIAL

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## الخلاصة :

لقد أستعمل نموذج بالاش وزيفل لكثافة الفراغ الفرميوني النصف تقليدي لحساب توابع الكثافة الموضعية ل مختلف مضاريب العزم  $p^n$ . فوجدنا أن توابع التوزع  $D_n$  تتناسب مع تحويل وايل في المربعة  $(n+3)/2$  تابع أبي .

أى

$$D_n(r) = \frac{4\pi}{(2\pi\hbar)^3} \frac{\Gamma((n+5)/2)}{n+1} \left(\frac{2}{\sigma_{E_F}(r)}\right)^{(n+1)/2} \mathcal{W}_{(n+3)/2}\{Ai(r), B(E_F, r)\}$$

حيث  $\mathcal{W}_n$  تمثل تحويل وايل و

$$B(E_F, r) = \sigma_{E_F}(r) \cdot (V(r) - E_F)$$

وتمثل طاقة فرمي  $E_F$  و  $\sigma_{E_F}(r)$  عامل للتناسب محسوبا عند الطاقة  $E_F$  وتمثل  $V(r)$ تابع الكون . ولذا فإن تابع توزيع الكثافة الرقيقة هو  $D_2(r)$  وتتابع توزيع كثافة الطاقة الحركية هو  $\frac{1}{2}m D_4(r)$

لقد حسبت القيم العددية للتكامل في تحويل وايل من أجل  $n=0, \frac{1}{2}, 1, \frac{3}{2}, \dots, 8$  ول  $B \in [2, 7.9]$  بدقة خمسة مراتب وجدولت في آخر هذا الموضوع .

لقد طبقنا هذه العملية على حالة جسم واحد عدم الالتفاف في كمون وود — ساكسون . وقد قورنت نتائج استخدام عوامل تتناسب ثابتة مع نتائج استخدام نموذج توماس — فرمي التقليدي .

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## ABSTRACT

The Balazs and Zipfel model for the semi-classical fermion  $\mu$ -space density is used to calculate spatial density functions for different powers of the momentum. We find that the distribution functions for  $p^n$ , are to a multiplicative factor, the Weyl transform of order  $(n+3)/2$  of the Airy function. Or,

$$D_n(r) = \frac{4\pi}{(2\pi\hbar)^3} \frac{\Gamma[(n+5)/2]}{n+1} \left( \frac{2}{\sigma_{E_F}(r)} \right)^{(n+1)/2} {}_{(n+3)/2}\{Ai(r), B(E_F, r)\}$$

where  $\mathcal{W}_u$  is the Weyl transform, and

$$B(E_F, r) = \sigma_{E_F}(r) \cdot (V(r) - E_F);$$

$E_F$  is the Fermi energy,  $\sigma_{E_F}(r)$  is a scaling factor evaluated at  $E_F$  and  $V(r)$  is the potential. Thus, the number density distribution function is  $D_2(r)$  and the kinetic energy density function is  $\frac{1}{2}m D_4(r)$ .

Tables of numerical values of the integral in the Weyl Transform for  $n=0, 1/2, 0, 3/2, \dots, 8$  and  $B \in [-7.9, 2]$ , accurate to five significant figures are presented.

We apply this procedure for the case of a spin-independent single-particle Woods-Saxon potential. Results for constant scaling factors are presented and compared to those of the classical Thomas-Fermi model.

## APPLICATION OF THE SEMI-CLASSICAL FERMION $\mu$ -SPACE DENSITY TO NUCLEI WOODS-SAXON POTENTIAL

### 1. INTRODUCTION

The Wigner transform of the singlet-density matrix [1–3] has had a wide range of applications in nuclear physics in recent years. For example, the Wigner density function, as it is usually referred to, has been used in a model for the relativistic transport in multi-particle production [4] to obtain a generalized master equation for relative and internal motions in deep-inelastic heavy-ion collisions [5] and to obtain semi-classical  $\mu$ -space for a dense Fermi gas [6]. The Wigner distribution function associated with the singlet-density matrix,  $\langle x_1 | \rho | x_2 \rangle$  is given by [7]

$$f(\mathbf{r}, \mathbf{p}) = \frac{1}{(2\pi)^3} \int d^3x \langle \mathbf{r} - \frac{\mathbf{x}}{2} | \rho | \mathbf{r} + \frac{\mathbf{x}}{2} \rangle \exp(-i\mathbf{p} \cdot \mathbf{x}), \quad (m=1, h=1) \quad (1)$$

The Wigner transform,  $f(\mathbf{r}, \mathbf{p})$ , corresponds to the semi-classical  $\mu$ -space, and can be regarded as a probability distribution for the coordinate  $\mathbf{r}$  and the momentum  $\mathbf{p}$ . Balazs and Zipfel [6] have obtained an approximate form for this function for a three-dimensional Fermi gas in a spherically symmetric potential well. Their result for an Airy-type approximation of the wave function is

$$f(r, p) = \frac{1}{(2\pi)^3} \int_{(H-E_F)\sigma}^{\infty} dt \text{Ai}(t) \quad (2)$$

where  $H(r, p) = \frac{1}{2}p^2 + V(r)$  and  $\sigma$  is a scaling factor.

In Section 2 we use the form of the Wigner function given in Equation (2) to calculate the distribution functions for the different powers of the momentum  $p$ . In Section 3 we use a single-particle Woods-Saxon potential in the Hamiltonian to get the density functions for  $p^n$  using constant scaling factor  $\sigma$ . In Section 4 we compare the results for the number and the kinetic energy densities with those of the classical Thomas-Fermi theory.

### 2. SEMI-CLASSICAL DENSITY DISTRIBUTION

The Wigner transform,  $f(r, p)$ , when multiplied by  $d^3r d^3p$ , represents the probability distribution for the coordinate and momenta. Hence, we may regard the integral

$$\int_0^{\infty} d^3p p^n f(r, p) \quad (3)$$

as a semi-classical distribution function for the  $n$ th power of the momentum. Using  $f(r, p)$  in Equation (2), and  $d^3p = 4\pi p^2 dp$ , the energy distribution functions for the  $(n-2)$ th power of the momentum will be given by:

$$D_n(r) = \frac{4\pi}{(2\pi)^3} \int_0^{\infty} dp p^n \int_{\sigma(1/2p^2 + V(r) - E_F)}^{\infty} dt \text{Ai}(t) \quad (4)$$

where  $E_F$  is the Fermi energy. Interchanging the order of integration in Equation (4), we get

$$D_n(r) = \frac{4\pi}{(2\pi)^3} \int_{B(E_F, r)}^{\infty} dt \text{Ai}(t) \int_0^{\sqrt{(2/\sigma(t-B))}} dp p^n \quad (5)$$

where  $B(E_F, r) = \sigma_{E_F}(r)(V(r) - E_F)$ . Or,

$$D_n(r) = \frac{4\pi}{(2\pi)^3} \frac{1}{n+1} \left( \frac{2}{\sigma_E(r)} \right)^{(n+1)/2} \int_B^{\infty} dt \text{Ai}(t) (t-B)^{(n+1)/2} \quad (6)$$

The Weyl (fractional) transform of order  $\mu$ , of a function  $f(x)$ , is defined as [8]

$$\mathcal{W}_\mu \{f(x); y\} = h(y; v) =$$

$$= \frac{1}{\Gamma(v)} \int_y^{\infty} f(x) (x-y)^{v-1} dx \quad (7)$$

The integral in Equation (6) has the same form as the Weyl transform of order  $\frac{1}{2}(n+3)$  of the Airy function. Thus, to a multiplicative factor the number density is proportional to the Weyl transform of order  $5/2$  of the Airy function and the kinetic energy density is proportional to the Weyl transform of order  $7/2$ . Or,

$$D_n(r) = \frac{4\pi}{(2\pi\hbar)^3} \frac{\Gamma[(n+5)/2]}{n+1} \left( \frac{2}{\sigma_{E_F}(r)} \right)^{(n+1)/2} {}_{(n+3)/2} \{ \text{Ai}(t); B(E_F, r) \} \quad (8)$$

The Weyl transforms are connected with differentiation [8]:

$$-\frac{d}{dy} h(y; \mu) = h(y; \mu - 1) \quad (9)$$

Thus, as in the classical Thomas-Fermi theory, the differentiation of the kinetic energy density with re-

spect to the energy,  $\sigma(E_F - V(r))$ , would result in a term proportional to the number density [9]. This result is consistent with the fact that should we replace the Airy function in the Wigner transform with a Heaviside step function, we would have the results of the classical Thomas-Fermi theory [6]. Other properties of the Wyle transform are [8]:

$$h(y; 1) = \int_y^\infty f(x) dx \quad (10)$$

and

$$\mathcal{W}_\mu \mathcal{W}_v = \mathcal{W}_{\mu+v} \quad (11)$$

or

$$\begin{aligned} & \frac{1}{\Gamma(\mu+v)} \int_y^\infty f(x) (x-y)^{\mu+v-1} dx \\ &= \frac{1}{\Gamma(\mu)} \frac{1}{\Gamma(v)} \int_y^\infty \left[ \int_x^\infty f(t)(t-x)^{v-1} dt \right] (x-y)^{\mu-1} dx \end{aligned}$$

to relate the energy density to the number density we set  $v=5/2$  and  $\mu=1$ . We get

$$D_4(r) = \frac{21}{5} \frac{1}{\sigma_{E_F}(r)} \int_{B(E_F, r)}^\infty D_2(t) dt \quad (12)$$

as the relation between the energy density and the number density.

The densities in Equation (8) have a functional dependence on the potential which appears both in the

limits of the integration  $B(E_F, r) = \sigma_{E_F}(r)(V(r) - E_F)$  and in the scaling factor  $\sigma$  as will be discussed in Section 3. The dependence of the number density on the potential warrant further consideration. For inasmuch as the potential is the result of the fermions and their distribution, self-consistency may be achieved by repeated application of the Weyl transform to the number density [10].

### 3. RESULTS FOR WOODS-SAXON POTENTIAL

The scaling factor in Equation (4) is given by [6]

$$\sigma(E, r) = \frac{2^{5/3}}{k_\parallel^2} \left( \frac{3S_\parallel}{2} \right)^2 \quad (13)$$

where

$$S_\parallel(r) = \int_r^{r_t} d\xi k_\parallel(\xi),$$

and

$$k_\parallel(\xi)^2 = 2 \left( E_{nl} - V(\xi) - \frac{(l + \frac{1}{2})^2}{2\xi^2} \right) \quad (14)$$

$r_t$  is the turning point and  $E_{nl}$  is the energy specified by the Bohr-Sommerfeld quantization rules.

Using a Woods-Saxon potential,  $V(r) = \frac{V_0}{1 + \exp[(r-a)/R]}$ , in Equation (14), we find that,

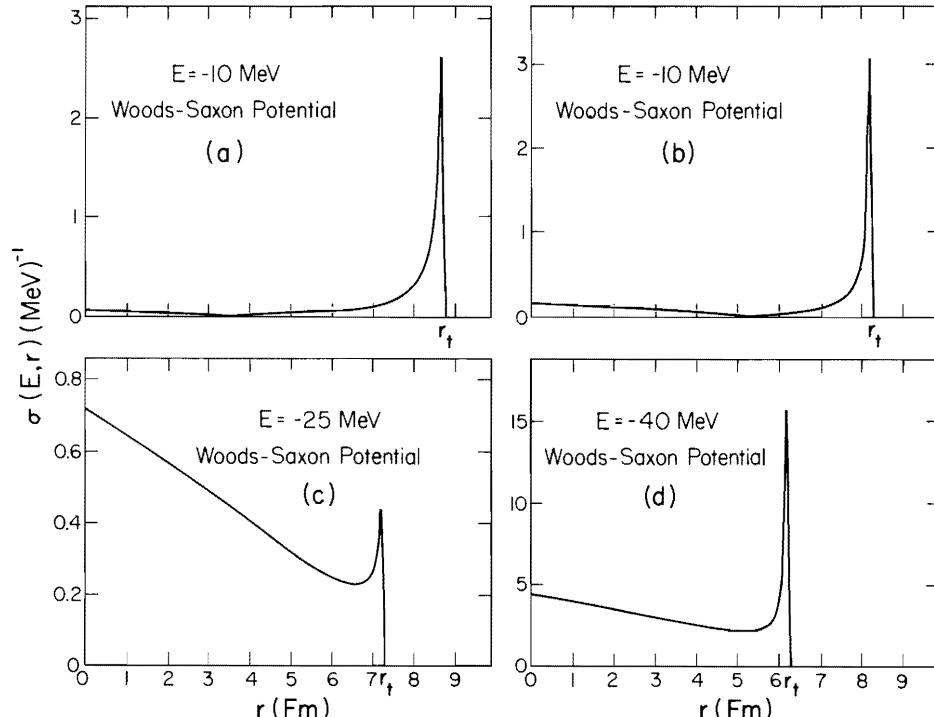


Figure 1. Scaling Factors of Equation (15) for a Woods-Saxon potential

should we ignore the  $(l + \frac{1}{2})^2/r^2$  term, the integral reduces to:

$$\sigma(E, r) = 2^{5/3} \left\{ \frac{3a}{(-2E)y^3} \left( \tan^{-1} y + \frac{1}{2y_0} \ln \frac{y_0 - y}{y_0 + y} \right) \right\}^{2/3} \quad (15)$$

where

$$y(E, r) = \sqrt{\left(\frac{V(r)}{E} - 1\right)} \quad \text{and} \quad y_0 = \sqrt{\left(\frac{V_0}{E} - 1\right)}$$

In Figure 1 we present plots of the scaling factor  $\sigma$ , Equation (15), as a function of the coordinates. In these plots we used  $V_0 = -47.1$  MeV,  $R = 7.36$  Fm,  $a = 0.66$  Fm in the Woods-Saxon potential. These numbers are consistent with neutrons in  $^{208}\text{Pb}$  [11]. Since the scaling factors presented in Figure 1 vanish at some coordinate position for the higher energies, we used a constant scaling factor  $\sigma_F = 2/(V'_F)^{2/3}$ , where  $V'_F$  is the derivative of the potential

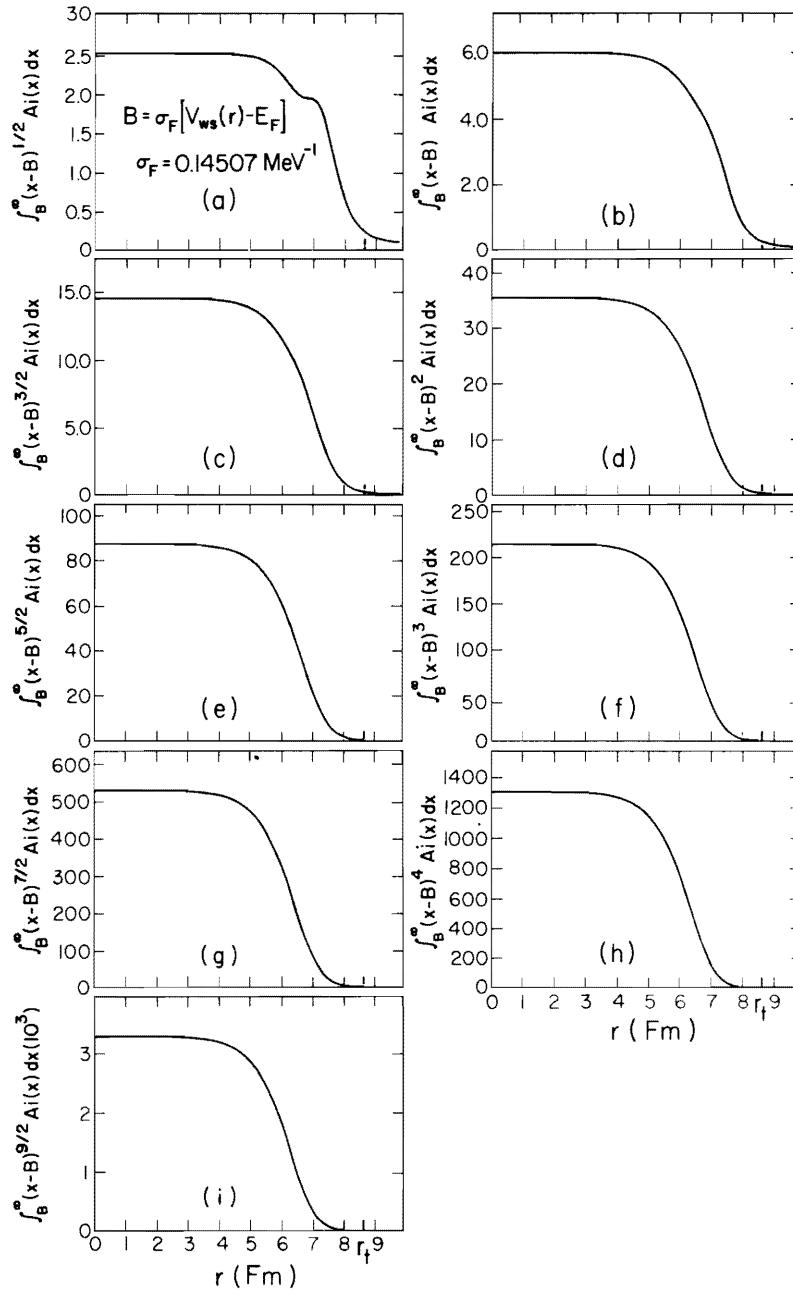


Figure 2. The Integral  $I_v(r) = \int_B^\infty (x-B)^v \text{Ai}(x)dx$ ,  $B = \sigma_F[V_{ws}(r) - E_F]$  with  $\sigma_F = 0.14506$  MeV $^{-1}$  for  $v = 1/2, 1, \dots, 9/2$

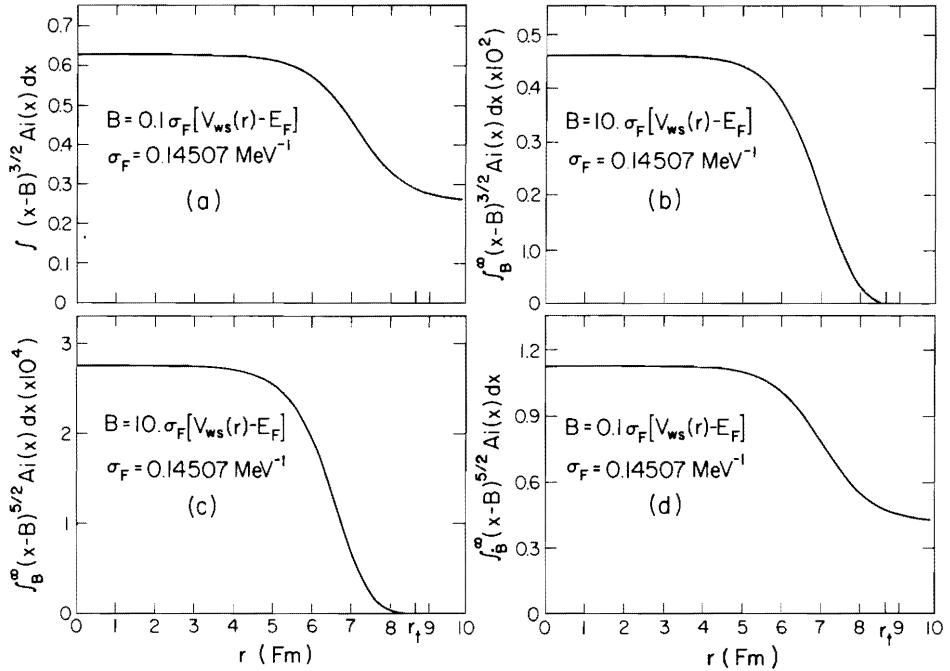


Figure 3. The integral  $I_{3/2}$  for the Number Density, and the integral  $I_{5/2}$  for the Kinetic Energy Density, Using  $\sigma = 0.1 \sigma_F$  and  $\sigma = 10.0 \sigma_F$ , and using a Woods-Saxon Potential

evaluated at the Fermi energy,  $E_F = -6$  MeV [11]. The value of  $\sigma_F$  used was  $0.14507 \text{ MeV}^{-1}$ .

In Figure 2 we present plots of the integrals

$$I_v(r) = \int_B^\infty (x-B)^v \text{Ai}(x) dx \quad B = \sigma_F [V_{ws}(r) - E_F] \quad (16)$$

for  $v = 1/2, 1, 3/2, \dots, 9/2$ , for Woods-Saxon potential and constant  $\sigma = \sigma_F$ . In Figure 3 we used  $\sigma_1 = 0.1 \sigma_F$  and  $\sigma_2 = 10.0 \sigma_F$  to calculate the integrals  $I_v$  in the number and energy densities. Other density distributions show similar trends as those in Figure 3.

Equations (9) and (12) represent the relation between integrals  $I_v$  with powers differing by one. In Figure 4 we plot the ratio of the integrals  $I_v/I_{v-1}$  for  $v = 1, 3/2$  using the same Woods-Saxon potential.

#### 4. DISCUSSION

In the Thomas-Fermi (TF) theory, the Wigner function is a step function which has a constant value,  $1/(2\pi\hbar)^3$ , in the classically allowed region and vanishes for higher energies. In Figure 5 we present the TF number and energy distributions for a Woods-Saxon potential. The Balazs and Zipfel (BZ) model replaces the step function with the integral of the Airy function. The integral of the Airy function, Figure 6, has a lower

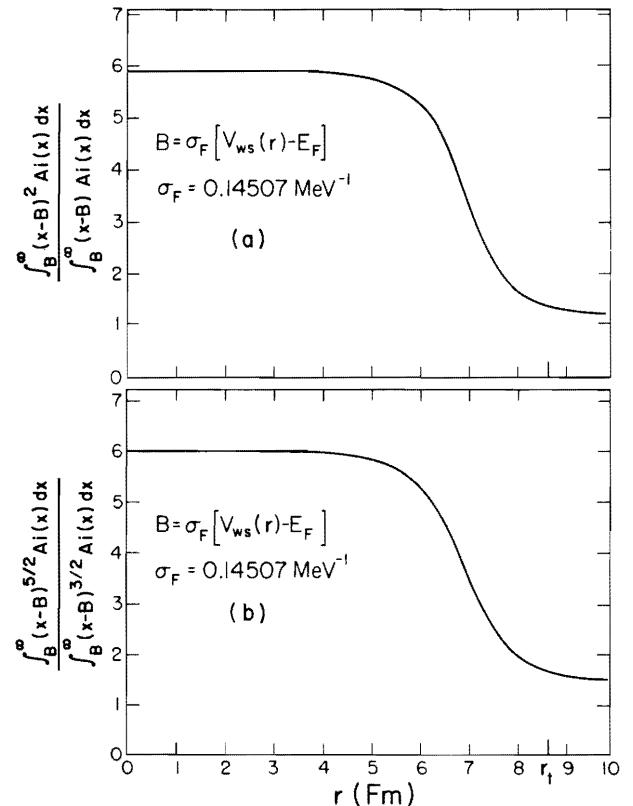


Figure 4. Ratios of the Integrals  $I_v^{(r)}/I_{v-1}^{(r)}$  for  $v = 1, 3/2$  Using a Woods-Saxon potential

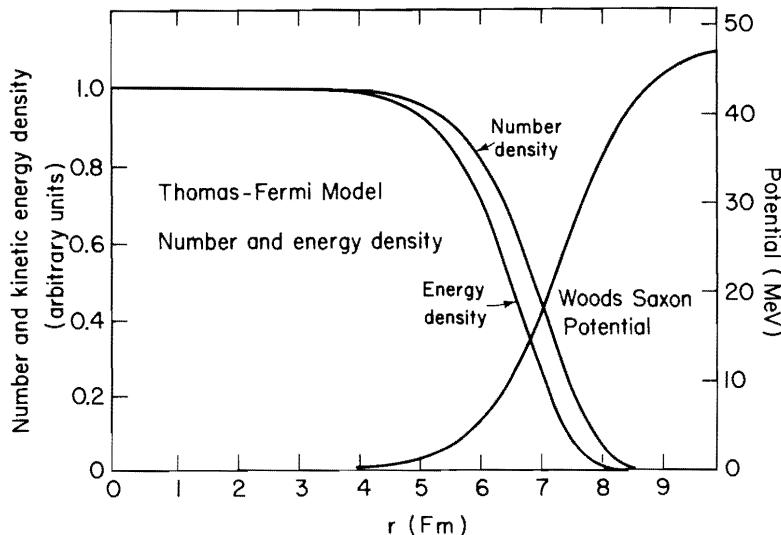


Figure 5. The Thomas-Fermi Number and Kinetic Energy distributions for a Woods-Saxon Potential,  $r_t$  = Turning Point

value,  $1/3$ , at the boundary of the classically forbidden region and oscillates about one in the interior region. In Table 1 we compare  $[E_F - V_{ws}(r)]^{3/2}$  and  $I_{3/2}(r)$  using  $B = \sigma_F [V_{ws}(r) - E_F]$ , which are involved in the number density in the TF and BZ cases, respectively. In Table 2 we compare  $[E_F - V_{ws}(r)]^{5/2}$  and the  $I_{5/2}$  integral. The term  $[E_F - V_{ws}(r)]^{5/2}$  represents the uncorrected kinetic energy density in the Thomas-Fermi theory [12] and  $I_{5/2}$  is proportional to the kinetic energy density in the Balazs and Zipfel model.

In the above we have used a single-particle Woods-Saxon potential to obtain the distribution functions for  $p^n$ . The addition of velocity-dependent terms to the potential could be handled easily provided an inverse to the limit of the integration in Equation (4) could be

found. It is interesting to note that should the dependence on the velocity be proportional to  $p^2$ , its effect will be the same as a change in the scaling factor  $\sigma$ .

Balazs and Pauli [13], have recently extended the model used above to include spin-dependent forces. Thus, for the case of spin one-half particles with spin-orbit interaction, the Wigner function we used would be replaced by a matrix in the spin indices. This matrix, the  $\mu$ -matrix, is a function of the semiclassical coordinate and momentum variables.

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#### APPENDIX

In Table 3, we present values of the integral

$$I_\nu(x) = \int_x^\infty (y-x)^\nu \text{Ai}(y) dy$$

for  $\nu = 1/2, 1, 3/2, \dots, 8$  and  $x \in [-7.9, 2]$ .

The Airy function was generated from an expansion with an accuracy of  $1 \times 10^{-10}$ , and we used the Romberg integration method with a relative error of  $1 \times 10^{-5}$ . Plots of the integrals are presented in Figure 7.

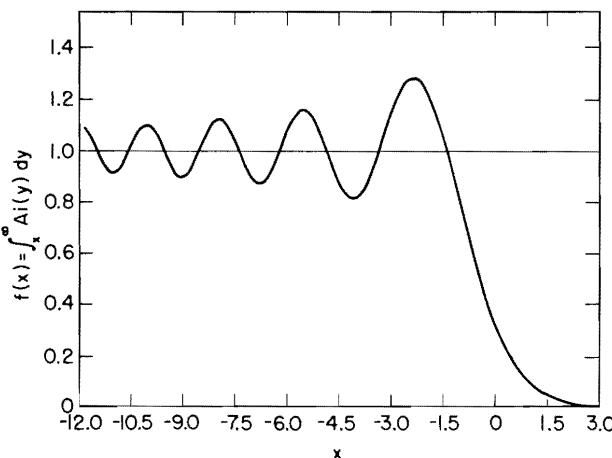


Figure 6. The Integral of the Airy Function

**Table 1. Number Densities**

$r(\text{Fm})$	Thomas = Fermi $[E_F - V_{ws}(r)]^{3/2}$	Balazs = Zipfel $\int_B^{\infty} (x - B)^{3/2} \text{Ai}(x) dx;$ $B = \sigma_F [V_{ws}(r) - E_F]$
0	$2.6348 \times 10^2$	$1.4554 \times 10^1$
1.0	$2.6160 \times 10^2$	$1.4553 \times 10^1$
2.0	$2.6336 \times 10^2$	$1.4547 \times 10^1$
3.0	$2.6288 \times 10^2$	$1.4520 \times 10^1$
4.0	$2.6072 \times 10^2$	$1.4396 \times 10^1$
5.0	$2.5125 \times 10^2$	$1.3855 \times 10^1$
6.0	$2.1401 \times 10^2$	$1.1755 \times 10^1$
7.0	$1.1624 \times 10^2$	$6.4754 \times 10^0$
7.2	$9.2076 \times 10^1$	$5.042 \times 10^0$
7.4	$6.9085 \times 10^1$	$3.6511 \times 10^0$
7.6	$4.8585 \times 10^1$	$2.4693 \times 10^0$
7.8	$3.1520 \times 10^1$	$1.5921 \times 10^0$
8.0	$1.8321 \times 10^1$	$1.0087 \times 10^0$
8.2	$8.9324 \times 10^0$	$6.4759 \times 10^{-1}$
8.4	$2.9843 \times 10^0$	$4.3161 \times 10^{-1}$
8.6	$1.1910 \times 10^{-1}$	$3.0294 \times 10^{-1}$
8.8	0	$2.2508 \times 10^{-1}$
9.0	0	$1.7674 \times 10^{-1}$
9.2	0	$1.4584 \times 10^{-1}$
9.4	0	$1.2553 \times 10^{-1}$
9.6	0	$1.1184 \times 10^{-1}$
9.8	0	$1.0243 \times 10^{-1}$

$$r_t = 8.63 \text{ Fm}$$

**Table 2.** Kinetic Energy Density

$r(\text{Fm})$	$\frac{\text{TF}}{[E_F - V_{\text{WS}}(r)]^{3/2}}$	$\int_B^x (x - B)^{5/2} \text{Ai}(z) dz; \\ B = \sigma_F [V_{\text{WS}}(r) - E_F]$
0	$1.0829 \times 10^4$	$8.7003 \times 10^1$
1.0	$1.0827 \times 10^4$	$8.6991 \times 10^1$
2.0	$1.0820 \times 10^4$	$8.6933 \times 10^1$
3.0	$1.0788 \times 10^4$	$8.6672 \times 10^1$
4.0	$1.0641 \times 10^4$	$8.5495 \times 10^1$
5.0	$1.0004 \times 10^4$	$8.0400 \times 10^1$
6.0	$7.6569 \times 10^3$	$6.1667 \times 10^1$
7.0	$2.7686 \times 10^3$	$2.2421 \times 10^1$
7.2	$1.8775 \times 10^3$	$1.5267 \times 10^1$
7.4	$1.1631 \times 10^3$	$9.6809 \times 10^0$
7.6	$6.4689 \times 10^2$	$5.7978 \times 10^0$
7.8	$3.1452 \times 10^2$	$3.3658 \times 10^0$
8.0	$1.2733 \times 10^2$	$1.9553 \times 10^0$
8.2	$3.8454 \times 10^1$	$1.1711 \times 10^0$
8.4	$6.1858 \times 10^0$	$7.3911 \times 10^{-1}$
8.6	$2.8832 \times 10^{-2}$	$4.9740 \times 10^{-1}$
8.8	0	$3.5789 \times 10^{-1}$
9.0	0	$2.7427 \times 10^{-1}$
9.2	0	$2.2222 \times 10^{-1}$
9.4	0	$1.8868 \times 10^{-1}$
9.6	0	$1.6640 \times 10^{-1}$
9.8	0	$1.5124 \times 10^{-1}$

 $r_t = 8.63 \text{ Fm}$

**Table 3a.** The Integral  $I_v(x) = \int_x^\infty (z-x)^v \text{Ai}(z) dz$  ( $v = 1/2, 1, 3/2, 2$ )

$x$	$I_{1/2}(x)$	$I_1(x)$	$I_{3/2}(x)$	$I_2(x)$
-7.9	2.84706(0)	7.89113(0)	2.21704(+1)	6.23816(+1)
-7.8	2.81371(0)	7.77970(0)	2.17458(+1)	6.08145(+1)
-7.7	2.77835(0)	7.66960(0)	2.13263(+1)	5.92696(+1)
-7.6	2.74233(0)	7.56162(0)	2.09123(+1)	5.77466(+1)
-7.5	2.70700(0)	7.45641(0)	2.05036(+1)	5.62448(+1)
-7.4	2.67367(0)	7.35439(0)	2.01001(+1)	5.47638(+1)
-7.3	2.64347(0)	7.25576(0)	1.97013(+1)	5.33028(+1)
-7.2	2.61728(0)	7.16047(0)	1.93069(+1)	5.18613(+1)
-7.1	2.59568(0)	7.06823(0)	1.89159(+1)	5.04384(+1)
-7.0	2.57893(0)	6.97850(0)	1.85279(+1)	4.90338(+1)
-6.9	2.56690(0)	6.89061(0)	1.81420(+1)	4.76469(+1)
-6.8	2.55914(0)	6.80373(0)	1.77576(+1)	4.62775(+1)
-6.7	2.55494(0)	6.71697(0)	1.73741(+1)	4.49254(+1)
-6.6	2.55326(0)	6.62944(0)	1.69910(+1)	4.35908(+1)
-6.5	2.55298(0)	6.54027(0)	1.66080(+1)	4.22737(+1)
-6.4	2.55282(0)	6.44874(0)	1.62251(+1)	4.09748(+1)
-6.3	2.55155(0)	6.35425(0)	1.58422(+1)	3.96944(+1)
-6.2	2.54796(0)	6.25641(0)	1.64597(+1)	3.84333(+1)
-6.1	2.54101(0)	6.15502(0)	1.50780(+1)	3.71921(+1)
-6.0	2.52987(0)	6.05012(0)	1.46977(+1)	3.59716(+1)
-5.9	2.51394(0)	5.94194(0)	1.43193(+1)	3.47723(+1)
-5.8	2.49290(0)	5.83092(0)	1.39437(+1)	3.35950(+1)
-5.7	2.46678(0)	5.71767(0)	1.35717(+1)	3.24401(+1)
-5.6	2.43570(0)	5.60292(0)	1.32040(+1)	3.13080(+1)
-5.5	2.40030(0)	5.48749(0)	1.28412(+1)	3.01990(+1)
-5.4	2.36134(0)	5.37223(0)	1.24841(+1)	2.91130(+1)
-5.3	2.31972(0)	5.25801(0)	1.21329(+1)	2.80500(+1)
-5.2	2.27649(0)	5.14559(0)	1.17882(+1)	2.70097(+1)
-5.1	2.23276(0)	5.03570(0)	1.14500(+1)	2.59916(+1)
-5.0	2.18966(0)	4.92888(0)	1.11184(+1)	2.49952(+1)
-4.9	2.14824(0)	4.82556(0)	1.07930(+1)	2.40198(+1)
-4.8	2.10948(0)	4.72597(0)	1.04738(+1)	2.30647(+1)
-4.7	2.07419(0)	4.63017(0)	1.01600(+1)	2.21292(+1)
-4.6	2.04299(0)	4.53802(0)	9.85129(0)	2.12124(+1)
-4.5	2.01631(0)	4.44924(0)	9.54690(0)	2.03137(+1)
-4.4	1.99434(0)	4.36336(0)	9.24616(0)	1.94325(+1)
-4.3	1.97707(0)	4.27982(0)	8.94836(0)	1.85682(+1)
-4.2	1.96424(0)	4.19792(0)	8.65281(0)	1.77205(+1)
-4.1	1.95544(0)	4.11691(0)	8.35887(0)	1.68890(+1)
-4.0	1.95005(0)	4.03599(0)	8.06600(0)	1.60737(+1)
-3.9	1.94730(0)	3.95438(0)	7.77372(0)	1.52746(+1)
-3.8	1.94633(0)	3.87129(0)	7.48171(0)	1.44920(+1)
-3.7	1.94622(0)	3.78602(0)	7.18974(0)	1.37263(+1)
-3.6	1.94599(0)	3.69795(0)	6.89785(0)	1.29778(+1)
-3.5	1.94470(0)	3.60653(0)	6.60603(0)	1.22473(+1)
-3.4	1.94140(0)	3.51137(0)	6.31454(0)	1.15355(+1)
-3.3	1.93525(0)	3.41219(0)	6.02375(0)	1.08430(+1)
-3.2	1.92548(0)	3.30885(0)	5.73416(0)	1.01709(+1)
-3.1	1.91146(0)	3.20134(0)	5.44633(0)	9.51978(0)
-3.0	1.89265(0)	3.08980(0)	5.16096(0)	8.89060(0)

Table 3a (continued)

$x$	$I_{1/2}(x)$	$I_1(x)$	$I_{3/2}(x)$	$I_2(x)$
-2.9	1.86868(0)	2.97449(0)	4.87880(0)	8.28411(0)
-2.8	1.83932(0)	2.85576(0)	4.60062(0)	7.70103(0)
-2.7	1.80449(0)	2.73409(0)	4.32727(0)	7.14200(0)
-2.6	1.76421(0)	2.61002(0)	4.05956(0)	6.60756(0)
-2.5	1.71866(0)	2.48418(0)	3.79828(0)	6.09811(0)
-2.4	1.66814(0)	2.35720(0)	3.54421(0)	5.61396(0)
-2.3	1.61303(0)	2.22981(0)	3.29807(0)	5.15526(0)
-2.2	1.55381(0)	2.10267(0)	3.06051(0)	4.72202(0)
-2.1	1.49102(0)	1.97650(0)	2.83211(0)	4.31413(0)
-2.0	1.42524(0)	1.85195(0)	2.61335(0)	3.93131(0)
-1.9	1.35709(0)	1.72968(0)	2.40465(0)	3.57319(0)
-1.8	1.28720(0)	1.61027(0)	2.20631(0)	3.23925(0)
-1.7	1.21621(0)	1.49427(0)	2.01854(0)	2.92886(0)
-1.6	1.14472(0)	1.38214(0)	1.84147(0)	2.64129(0)
-1.5	1.07332(0)	1.27431(0)	1.67512(0)	2.37572(0)
-1.4	1.00258(0)	1.17111(0)	1.51944(0)	2.13125(0)
-1.3	9.32989(-1)	1.07282(0)	1.37429(0)	1.90694(0)
-1.2	8.65007(-1)	9.79657(-1)	1.23946(0)	1.70178(0)
-1.1	7.99034(-1)	8.91746(-1)	1.11469(0)	1.51473(0)
-1.0	7.35414(-1)	8.09168(-1)	9.99634(-1)	1.34473(0)
-0.9	6.74431(-1)	7.31941(-1)	8.94215(-1)	1.19071(0)
-0.8	6.16314(-1)	6.60030(-1)	7.97160(-1)	1.05160(0)
-0.7	5.61232(-1)	5.99351(-1)	7.08882(-1)	9.26346(-1)
-0.6	5.09307(-1)	5.31779(-1)	6.28631(-1)	8.13917(-1)
-0.5	4.60609(-1)	4.75153(-1)	5.55928(-1)	7.13305(-1)
-0.4	4.15164(-1)	4.23283(-1)	4.90286(-1)	6.23539(-1)
-0.3	3.72958(-1)	3.75953(-1)	4.31216(-1)	5.43689(-1)
-0.2	3.33943(-1)	3.32931(-1)	3.78238(-1)	4.72870(-1)
-0.1	2.98040(-1)	2.93971(-1)	3.30878(-1)	4.10246(-1)
0.0	2.65146(-1)	2.58819(-1)	2.88675(-1)	3.55028(-1)
0.1	2.35138(-1)	2.27218(-1)	2.51189(-1)	3.06481(-1)
0.2	2.07875(-1)	1.98909(-1)	2.17996(-1)	2.63921(-1)
0.3	1.83208(-1)	1.73637(-1)	1.88696(-1)	2.26715(-1)
0.4	1.60977(-1)	1.51155(-1)	1.62912(-1)	1.94280(-1)
0.5	1.41019(-1)	1.31221(-1)	1.40289(-1)	1.66083(-1)
0.6	1.23169(-1)	1.13604(-1)	1.20500(-1)	1.41638(-1)
0.7	1.07263(-1)	9.80865(-2)	1.03241(-1)	1.20502(-1)
0.8	9.31412(-2)	8.44618(-2)	8.82321(-2)	1.02277(-1)
0.9	8.06472(-2)	7.25366(-2)	7.52173(-2)	8.66039(-2)
1.0	6.96317(-2)	6.21315(-2)	6.39639(-2)	7.31610(-2)
1.1	5.99528(-2)	5.30804(-2)	6.42609(-2)	6.16610(-2)
1.2	5.14768(-2)	4.52308(-2)	4.59178(-2)	5.18487(-2)
1.3	4.40784(-2)	3.84437(-2)	3.87639(-2)	4.34979(-2)
1.4	3.76414(-2)	3.25922(-2)	3.26462(-2)	3.64089(-2)
1.5	3.20587(-2)	2.74521(-2)	2.74287(-2)	3.04063(-2)
1.6	2.72318(-2)	2.32604(-2)	2.29908(-2)	2.53362(-2)
1.7	2.30712(-2)	1.95649(-2)	1.92258(-2)	2.10644(-2)
1.8	1.94957(-2)	1.64235(-2)	1.60401(-2)	1.74740(-2)
1.9	1.64322(-2)	1.37531(-2)	1.33515(-2)	1.44636(-2)
2.0	1.38151(-2)	1.14892(-2)	1.10881(-2)	1.19457(-2)

**Table 3b.** Values of the Integral  $I_v(x) = \int_x^\infty (z-x)^v \text{Ai}(z) dz$  ( $v=5/2, 3, 7/2, 4$ )

$x$	$I_{5/2}(x)$	$I_3(x)$	$I_{7/2}(x)$	$I_4(x)$
-7.9	1.75625(+2)	4.95051(+2)	1.39811(+3)	3.95825(+3)
-7.8	1.70135(+2)	4.76572(+2)	1.33761(+3)	3.76394(+3)
-7.7	1.64752(+2)	4.58560(+2)	1.27901(+3)	3.57693(+3)
-7.6	1.59472(+2)	4.41008(+2)	1.22227(+3)	3.39703(+3)
-7.5	1.54295(+2)	4.23909(+2)	1.16736(+3)	3.22406(+3)
-7.4	1.49220(+2)	4.07259(+2)	1.11425(+3)	3.05784(+3)
-7.3	1.44245(+2)	3.91049(+2)	1.06290(+3)	2.89819(+3)
-7.2	1.39369(+2)	3.75275(+2)	1.01327(+3)	2.74494(+3)
-7.1	1.34591(+2)	3.59931(+2)	9.65329(+2)	2.59792(+3)
-7.0	1.29910(+2)	3.45010(+2)	9.19044(+2)	2.45694(+3)
-6.9	1.25327(+2)	3.30509(+2)	8.74380(+2)	2.32185(+3)
-6.8	1.20839(+2)	3.16420(+2)	8.31304(+2)	2.19248(+3)
-6.7	1.16448(+2)	3.02740(+2)	7.89782(+2)	2.06866(+3)
-6.6	1.12152(+2)	2.89463(+2)	7.49779(+2)	1.95023(+3)
-6.5	1.07952(+2)	2.76584(+2)	7.11264(+2)	1.83704(+3)
-6.4	1.03848(+2)	2.64097(+2)	6.74202(+2)	1.72891(+3)
-6.3	9.98398(+1)	2.51997(+2)	6.38559(+2)	1.62571(+3)
-6.2	9.59270(+1)	2.40279(+2)	6.04303(+2)	1.52727(+3)
-6.1	9.21098(+1)	2.28935(+2)	5.71399(+2)	1.43344(+3)
-6.0	8.83879(+1)	2.17961(+2)	5.39814(+2)	1.34407(+3)
-5.9	8.47608(+1)	2.07350(+2)	5.09516(+2)	1.25902(+3)
-5.8	8.12280(+1)	1.97096(+2)	4.80471(+2)	1.17814(+3)
-5.7	7.77887(+1)	1.87191(+2)	4.52646(+2)	1.10130(+3)
-5.6	7.44418(+1)	1.77629(+2)	4.26008(+2)	1.02834(+3)
-5.5	7.11863(+1)	1.68404(+2)	4.00526(+2)	9.59147(+2)
-5.4	6.80208(+1)	1.59508(+2)	3.76167(+2)	8.93575(+2)
-5.3	6.49438(+1)	1.50934(+2)	3.52901(+2)	8.31498(+2)
-5.2	6.19537(+1)	1.42675(+2)	3.30696(+2)	7.72786(+2)
-5.1	5.90491(+1)	1.34726(+2)	3.09523(+2)	7.17316(+2)
-5.0	5.62282(+1)	1.27078(+2)	2.89352(+2)	6.64965(+2)
-4.9	5.34894(+1)	1.19727(+2)	2.70154(+2)	6.15614(+2)
-4.8	5.08312(+1)	1.12664(+2)	2.51900(+2)	5.69145(+2)
-4.7	4.82521(+1)	1.05886(+2)	2.34563(+2)	5.25444(+2)
-4.6	4.57508(+1)	9.93851(+1)	2.18115(+2)	4.84399(+2)
-4.5	4.33261(+1)	9.31566(+1)	2.02528(+2)	4.45900(+2)
-4.4	4.09770(+1)	8.71951(+1)	1.87778(+2)	4.09839(+2)
-4.3	3.87027(+1)	8.14954(+1)	1.73836(+2)	3.76109(+2)
-4.2	3.65026(+1)	7.60525(+1)	1.60677(+2)	3.44608(+2)
-4.1	3.43762(+1)	7.08615(+1)	1.48275(+2)	3.15234(+2)
-4.0	3.23231(+1)	6.59175(+1)	1.36605(+2)	2.87886(+2)
-3.9	3.03432(+1)	6.12156(+1)	1.25641(+2)	2.62467(+2)
-3.8	2.84362(+1)	5.67511(+1)	1.15356(+2)	2.38882(+2)
-3.7	2.66023(+1)	5.25187(+1)	1.05727(+2)	2.17035(+2)
-3.6	2.48413(+1)	4.85136(+1)	9.67263(+1)	1.96836(+2)
-3.5	2.31534(+1)	4.47302(+1)	8.83294(+1)	1.78195(+2)
-3.4	2.15383(+1)	4.11633(+1)	8.05104(+1)	1.61023(+2)
-3.3	1.99960(+1)	3.78070(+1)	7.32441(+1)	1.45236(+2)
-3.2	1.85263(+1)	3.46555(+1)	6.65048(+1)	1.30751(+2)
-3.1	1.71288(+1)	3.17024(+1)	6.02672(+1)	1.17485(+2)
-3.0	1.58029(+1)	2.89414(+1)	5.45062(+1)	1.05363(+2)
-2.9	1.45480(+1)	2.63658(+1)	4.91969(+1)	9.43076(+1)

Table 3b (continued)

$x$	$I_{5/2}(x)$	$I_3(x)$	$I_{7/2}(x)$	$I_4(x)$
-2.8	1.33632(+1)	2.39686(+1)	4.43144(+1)	8.42466(+1)
-2.7	1.22473(+1)	2.17427(+1)	3.98346(+1)	7.51099(+1)
-2.6	1.11991(+1)	1.96809(+1)	3.57334(+1)	6.68305(+1)
-2.5	1.02170(+1)	1.77757(+1)	3.19875(+1)	5.93443(+1)
-2.4	9.29936(0)	1.60195(+1)	2.85740(+1)	5.25901(+1)
-2.3	8.44424(0)	1.44048(+1)	2.54706(+1)	4.65098(+1)
-2.2	7.64961(0)	1.29238(+1)	2.26560(+1)	4.10484(+1)
-2.1	6.91323(0)	1.15690(+1)	2.01091(+1)	3.61539(+1)
-2.0	6.23275(0)	1.03328(+1)	1.78102(+1)	3.17774(+1)
-1.9	5.60571(0)	9.20778(0)	1.57400(+1)	2.78729(+1)
-1.8	5.02956(0)	8.18651(0)	1.38802(+1)	2.43973(+1)
-1.7	4.50168(0)	7.26187(0)	1.22136(+1)	2.13108(+1)
-1.6	4.01940(0)	6.42691(0)	1.07237(+1)	1.85759(+1)
-1.5	3.58005(0)	5.67490(0)	9.39505(0)	1.61582(+1)
-1.4	3.18095(0)	4.99937(0)	8.21301(0)	1.40258(+1)
-1.3	2.81945(0)	4.39413(0)	7.16400(0)	1.21493(+1)
-1.2	2.49294(0)	3.85329(0)	6.23531(0)	1.05019(+1)
-1.1	2.19888(0)	3.37125(0)	5.41516(0)	9.05885(0)
-1.0	1.93479(0)	2.94274(0)	4.69260(0)	7.79775(0)
-0.9	1.69829(0)	2.56281(0)	4.05758(0)	6.69818(0)
-0.8	1.48708(0)	2.22683(0)	3.50085(0)	5.74164(0)
-0.7	1.29899(0)	1.93047(0)	3.01393(0)	4.91143(0)
-0.6	1.13197(0)	1.66974(0)	2.58909(0)	4.19252(0)
-0.5	9.84055(-1)	1.44094(0)	2.21932(0)	3.57139(0)
-0.4	8.53420(-1)	1.24067(0)	2.89824(0)	3.03596(0)
-0.3	7.38364(-1)	1.06582(0)	1.62011(0)	2.57546(0)
-0.2	6.37305(-1)	9.13555(-1)	1.37975(0)	2.18029(0)
-0.1	5.48777(-1)	7.81282(-1)	1.17253(0)	1.84195(0)
0.0	4.71436(-1)	6.66667(-1)	9.94302(-1)	1.55292(0)
0.1	4.04047(-1)	5.67598(-1)	8.41365(-1)	1.30655(0)
0.2	3.45484(-1)	4.82179(-1)	7.10439(-1)	1.09702(0)
0.3	2.94725(-1)	4.08710(-1)	5.98616(-1)	9.19212(-1)
0.4	2.50843(-1)	3.45673(-1)	5.03330(-1)	7.68660(-1)
0.5	2.13005(-1)	2.91718(-1)	4.22321(-1)	6.41464(-1)
0.6	1.80462(-1)	2.45648(-1)	3.53609(-1)	5.34235(-1)
0.7	1.52544(-1)	2.06405(-1)	2.95458(-1)	4.44035(-1)
0.8	1.28654(-1)	1.73056(-1)	2.46358(-1)	3.68325(-1)
0.9	1.08262(-1)	1.44784(-1)	2.04992(-1)	3.04914(-1)
1.0	9.08991(-2)	1.20871(-1)	1.70221(-1)	2.51917(-1)
1.1	7.61513(-2)	1.00693(-1)	1.41058(-1)	2.07720(-1)
1.2	6.36554(-2)	8.37057(-2)	1.16652(-1)	1.70938(-1)
1.3	5.30933(-2)	5.94376(-2)	9.62735(-2)	1.40393(-1)
1.4	4.41872(-2)	5.74808(-2)	7.92940(-2)	1.15080(-1)
1.5	3.66953(-2)	4.74837(-2)	6.51776(-2)	9.41470(-2)
1.6	3.04079(-2)	3.91439(-2)	5.34669(-2)	7.58721(-2)
1.7	2.51439(-2)	3.22022(-2)	4.37727(-2)	6.26457(-2)
1.8	2.07468(-2)	2.64372(-2)	3.57651(-2)	5.09576(-2)
1.9	1.70824(-2)	2.16599(-2)	2.91646(-2)	4.13644(-2)
2.0	1.40356(-2)	1.77098(-2)	2.37354(-2)	3.35156(-2)

**Table 3c. The Integral  $I_v(x) = \int_x^{\infty} (z-x)^v A(z) dz$  ( $v=9/2, 5, 11/2, 6$ )**

$x$	$I_{9/2}(x)$	$I_5(x)$	$I_{11/2}(x)$	$I_6(x)$
-7.9	1.12391(+4)	3.20187(+4)	9.15545(+4)	2.62849(+5)
-7.8	1.06236(+4)	3.00885(+4)	8.55439(+4)	2.44222(+5)
-7.7	1.00350(+4)	2.82536(+4)	7.98640(+4)	2.26724(+5)
-7.6	9.47223(+3)	2.65104(+4)	7.45007(+4)	2.10299(+5)
-7.5	8.93463(+3)	2.48554(+4)	6.94399(+4)	1.94894(+5)
-7.4	8.42134(+3)	2.32852(+4)	6.46681(+4)	1.80456(+5)
-7.3	7.93154(+3)	2.17964(+4)	6.01721(+4)	1.66935(+5)
-7.2	7.46447(+3)	2.03869(+4)	5.59392(+4)	1.54284(+5)
-7.1	7.01935(+3)	1.90505(+4)	5.19572(+4)	1.42457(+5)
-7.0	5.59543(+3)	1.77870(+4)	4.82141(+4)	1.31409(+5)
-6.9	6.19198(+3)	1.65925(+4)	4.46985(+4)	1.21099(+5)
-6.8	5.80825(+3)	1.54642(+4)	4.13993(+4)	1.11485(+5)
-6.7	5.44356(+3)	1.43991(+4)	3.83059(+4)	1.02529(+5)
-6.6	5.09721(+3)	1.33946(+4)	3.54080(+4)	9.41939(+4)
-6.5	4.76854(+3)	1.24480(+4)	3.26957(+4)	8.64439(+4)
-6.4	4.45686(+3)	1.15568(+4)	3.01595(+4)	7.92452(+4)
-6.3	4.16154(+3)	1.07183(+4)	2.77902(+4)	7.25652(+4)
-6.2	3.88196(+3)	9.93025(+3)	2.55789(+4)	6.63731(+4)
-6.1	3.61747(+3)	9.19026(+3)	2.35173(+4)	6.06393(+4)
-6.0	3.36749(+3)	8.49607(+3)	2.15971(+4)	5.53356(+4)
-5.9	3.13144(+3)	7.84548(+3)	1.98105(+4)	5.04353(+4)
-5.8	2.90874(+3)	7.23636(+3)	1.81500(+4)	4.59128(+4)
-5.7	2.69883(+3)	6.66666(+3)	1.66085(+4)	4.17438(+4)
-5.6	2.50118(+3)	6.13441(+3)	1.51791(+4)	3.79053(+4)
-5.5	2.31525(+3)	5.63769(+3)	1.38551(+4)	3.43754(+4)
-5.4	2.14054(+3)	5.17466(+3)	1.26302(+4)	3.11333(+4)
-5.3	1.97654(+3)	4.74354(+3)	1.14985(+4)	2.81594(+4)
-5.2	1.82277(+3)	4.34260(+3)	1.04542(+4)	2.54350(+4)
-5.1	1.67876(+3)	3.97021(+3)	9.49168(+3)	2.29426(+4)
-5.0	1.54405(+3)	3.62477(+3)	8.60583(+3)	2.06654(+4)
-4.9	1.41819(+3)	3.30475(+3)	7.79161(+3)	1.85878(+4)
-4.8	1.30077(+3)	3.00867(+3)	7.04427(+3)	1.66949(+4)
-4.7	1.19135(+3)	2.73514(+3)	6.35930(+3)	1.49729(+4)
-4.6	1.08953(+3)	2.48279(+3)	5.73240(+3)	1.34085(+4)
-4.5	9.94913(+2)	2.25032(+3)	5.15950(+3)	1.19896(+4)
-4.4	9.07125(+2)	2.03648(+3)	4.63674(+3)	1.07044(+4)
-4.3	8.25792(+2)	1.84009(+3)	4.16047(+3)	9.54229(+3)
-4.2	7.50556(+2)	1.66000(+3)	3.72725(+3)	8.49305(+3)
-4.1	6.81069(+2)	1.49513(+3)	3.33381(+3)	7.54724(+3)
-4.0	6.16998(+2)	1.34443(+3)	2.97708(+3)	6.69606(+3)
-3.9	5.58019(+2)	1.20692(+3)	2.65418(+3)	5.93129(+3)
-3.8	5.03819(+2)	1.08166(+3)	2.36238(+3)	5.24531(+3)
-3.7	4.54100(+2)	9.67746(+2)	2.09916(+3)	4.63104(+3)
-3.6	4.08571(+2)	8.64345(+2)	1.86211(+3)	4.08191(+3)
-3.5	3.66956(+2)	7.70650(+2)	1.64901(+3)	3.59188(+3)
-3.4	3.28988(+2)	6.85905(+2)	1.45779(+3)	3.15534(+3)
-3.3	2.94413(+2)	6.09396(+2)	1.28650(+3)	2.76715(+3)
-3.2	2.62989(+2)	5.40452(+2)	1.13335(+3)	2.42256(+3)
-3.1	2.34484(+2)	4.78442(+2)	9.96678(+2)	2.11722(+3)
-3.0	2.08677(+2)	4.22776(+2)	8.74928(+2)	1.84716(+3)
-2.9	1.85360(+2)	3.72901(+2)	7.66677(+2)	1.60873(+3)

Table 3c (continued)

$x$	$I_{9/2}(x)$	$I_5(x)$	$I_{11/2}(x)$	$I_6(x)$
-2.8	<b>1.64336(+2)</b>	<b>3.28303(+2)</b>	<b>6.70611(+2)</b>	<b>1.39862(+3)</b>
-2.7	<b>1.45417(+2)</b>	<b>2.88501(+2)</b>	<b>5.85521(+2)</b>	<b>1.21381(+3)</b>
-2.6	<b>1.28428(+2)</b>	<b>2.53050(+2)</b>	<b>5.10299(+2)</b>	<b>1.05155(+3)</b>
-2.5	<b>1.13204(+2)</b>	<b>2.21538(+2)</b>	<b>4.43927(+2)</b>	<b>9.09359(+2)</b>
-2.4	<b>9.95894(+1)</b>	<b>1.93584(+2)</b>	<b>3.85479(+2)</b>	<b>7.84991(+2)</b>
-2.3	<b>8.74406(+1)</b>	<b>1.68836(+2)</b>	<b>3.34110(+2)</b>	<b>6.76418(+2)</b>
-2.2	<b>7.66225(+1)</b>	<b>1.46971(+2)</b>	<b>2.89051(+2)</b>	<b>5.81812(+2)</b>
-2.1	<b>6.70101(+1)</b>	<b>1.27693(+2)</b>	<b>2.49604(+2)</b>	<b>4.99535(+2)</b>
-2.0	<b>5.84872(+1)</b>	<b>1.10731(+2)</b>	<b>2.15140(+2)</b>	<b>4.28118(+2)</b>
-1.9	<b>5.09466(+1)</b>	<b>9.58367(+1)</b>	<b>1.85088(+2)</b>	<b>3.66245(+2)</b>
-1.8	<b>4.42896(+1)</b>	<b>8.27862(+1)</b>	<b>1.58937(+2)</b>	<b>3.12745(+2)</b>
-1.7	<b>3.84254(+1)</b>	<b>7.13746(+1)</b>	<b>1.36225(+2)</b>	<b>2.66574(+2)</b>
-1.6	<b>3.32708(+1)</b>	<b>6.14168(+1)</b>	<b>1.16539(+2)</b>	<b>2.26805(+2)</b>
-1.5	<b>2.87499(+1)</b>	<b>5.27459(+1)</b>	<b>9.95106(+1)</b>	<b>1.92617(+2)</b>
-1.4	<b>2.47933(+1)</b>	<b>4.52111(+1)</b>	<b>8.48106(+1)</b>	<b>1.63283(+2)</b>
-1.3	<b>2.13382(+1)</b>	<b>3.86774(+1)</b>	<b>7.21460(+1)</b>	<b>1.38163(+2)</b>
-1.2	<b>1.83277(+1)</b>	<b>3.30237(+1)</b>	<b>6.12571(+1)</b>	<b>1.16694(+2)</b>
-1.1	<b>1.57102(+1)</b>	<b>2.81415(+1)</b>	<b>5.19136(+1)</b>	<b>9.83806(+1)</b>
-1.0	<b>1.34394(+1)</b>	<b>2.39345(+1)</b>	<b>4.39123(+1)</b>	<b>8.27893(+1)</b>
-0.9	<b>1.14737(+1)</b>	<b>2.03168(+1)</b>	<b>3.70743(+1)</b>	<b>6.95414(+1)</b>
-0.8	<b>9.77582(0)</b>	<b>1.72125(+1)</b>	<b>3.12422(+1)</b>	<b>5.83065(+1)</b>
-0.7	<b>8.31247(0)</b>	<b>1.45542(+1)</b>	<b>2.62780(+1)</b>	<b>4.87972(+1)</b>
-0.6	<b>7.05398(0)</b>	<b>1.22825(+1)</b>	<b>2.20609(+1)</b>	<b>4.07642(+1)</b>
-0.5	<b>5.97403(0)</b>	<b>1.03453(+1)</b>	<b>1.84859(+1)</b>	<b>3.39914(+1)</b>
-0.4	<b>5.04929(0)</b>	<b>8.69684(0)</b>	<b>1.54611(+1)</b>	<b>2.82921(+1)</b>
-0.3	<b>4.25917(0)</b>	<b>7.29690(0)</b>	<b>1.29070(+1)</b>	<b>2.35055(+1)</b>
-0.2	<b>3.58553(0)</b>	<b>6.11050(0)</b>	<b>1.07546(+1)</b>	<b>1.94931(+1)</b>
-0.1	<b>3.01243(0)</b>	<b>5.10714(0)</b>	<b>8.94449(0)</b>	<b>1.61363(+1)</b>
0.0	<b>2.52591(0)</b>	<b>4.26033(0)</b>	<b>7.42511(0)</b>	<b>1.33333(+1)</b>
0.1	<b>2.11377(0)</b>	<b>3.54712(0)</b>	<b>6.15235(0)</b>	<b>1.09972(+1)</b>
0.2	<b>1.76538(0)</b>	<b>2.94765(0)</b>	<b>5.08829(0)</b>	<b>9.05402(0)</b>
0.3	<b>1.47151(0)</b>	<b>2.44482(0)</b>	<b>4.20045(0)</b>	<b>7.44072(0)</b>
0.4	<b>1.22414(0)</b>	<b>2.02390(0)</b>	<b>3.46112(0)</b>	<b>6.10387(0)</b>
0.5	<b>1.01637(0)</b>	<b>1.67227(0)</b>	<b>2.84664(0)</b>	<b>4.99820(0)</b>
0.6	<b>8.42212(-1)</b>	<b>1.37911(0)</b>	<b>2.33695(0)</b>	<b>4.08547(0)</b>
0.7	<b>6.96538(-1)</b>	<b>1.13519(0)</b>	<b>1.91499(0)</b>	<b>3.33343(0)</b>
0.8	<b>5.74943(-1)</b>	<b>9.32660(-1)</b>	<b>1.56634(0)</b>	<b>2.71497(0)</b>
0.9	<b>4.73657(-1)</b>	<b>7.64821(-1)</b>	<b>1.27883(0)</b>	<b>2.20731(0)</b>
1.0	<b>3.89462(-1)</b>	<b>6.26012(-1)</b>	<b>1.04219(0)</b>	<b>1.79138(0)</b>
1.1	<b>3.19618(-1)</b>	<b>5.11438(-1)</b>	<b>8.47795(-1)</b>	<b>1.45125(0)</b>
1.2	<b>2.61797(-1)</b>	<b>4.17057(-1)</b>	<b>6.88409(-1)</b>	<b>1.17362(0)</b>
1.3	<b>2.14027(-1)</b>	<b>3.39462(-1)</b>	<b>5.57978(-1)</b>	<b>9.47431(-1)</b>
1.4	<b>1.74642(-1)</b>	<b>2.75793(-1)</b>	<b>4.51444(-1)</b>	<b>7.63487(-1)</b>
1.5	<b>1.42234(-1)</b>	<b>2.23653(-1)</b>	<b>3.64594(-1)</b>	<b>6.14176(-1)</b>
1.6	<b>1.15621(-1)</b>	<b>1.81037(-1)</b>	<b>2.93925(-1)</b>	<b>4.93201(-1)</b>
1.7	<b>9.38114(-2)</b>	<b>1.46273(-1)</b>	<b>2.36531(-1)</b>	<b>3.95364(-1)</b>
1.8	<b>7.59731(-2)</b>	<b>1.17969(-1)</b>	<b>1.90005(-1)</b>	<b>3.16383(-1)</b>
1.9	<b>6.14120(-2)</b>	<b>9.49694(-2)</b>	<b>1.52360(-1)</b>	<b>2.52741(-1)</b>
2.0	<b>4.95494(-2)</b>	<b>7.63152(-2)</b>	<b>1.21958(-1)</b>	<b>2.01552(-1)</b>

**Table 3d.** The Integral  $I_v(x) = \int_x^\infty (z-x)^v \text{Ai}(z) dz$  ( $v = 13/2, 7, 15/2, 8$ )

$x$	$I_{13/2}(x)$	$I_7(x)$	$I_{15/2}(x)$	$I_8(x)$
-7.9	<b>7.578 87(+5)</b>	<b>2.195 25(+6)</b>	<b>6.389 10(+6)</b>	<b>1.868 73(+7)</b>
-7.8	<b>7.003 48(+5)</b>	<b>2.017 85(+6)</b>	<b>5.842 51(+6)</b>	<b>1.700 29(+7)</b>
-7.7	<b>6.466 08(+5)</b>	<b>1.853 08(+6)</b>	<b>5.337 63(+6)</b>	<b>1.545 54(+7)</b>
-7.6	<b>5.964 56(+5)</b>	<b>1.700 18(+6)</b>	<b>4.871 70(+6)</b>	<b>1.403 48(+7)</b>
-7.5	<b>5.496 92(+5)</b>	<b>1.558 42(+6)</b>	<b>4.442 10(+6)</b>	<b>1.273 21(+7)</b>
-7.4	<b>5.061 22(+5)</b>	<b>1.427 11(+6)</b>	<b>4.046 36(+6)</b>	<b>1.153 86(+7)</b>
-7.3	<b>4.655 63(+5)</b>	<b>1.305 57(+6)</b>	<b>3.682 16(+6)</b>	<b>1.044 61(+7)</b>
-7.2	<b>4.278 41(+5)</b>	<b>1.193 19(+6)</b>	<b>3.347 31(+6)</b>	<b>9.447 20(+6)</b>
-7.1	<b>3.927 88(+5)</b>	<b>1.089 38(+6)</b>	<b>3.039 74(+6)</b>	<b>8.534 73(+6)</b>
-7.0	<b>3.602 45(+5)</b>	<b>9.935 73(+5)</b>	<b>2.757 50(+6)</b>	<b>7.702 06(+6)</b>
-6.9	<b>3.300 60(+5)</b>	<b>9.052 37(+5)</b>	<b>2.498 78(+6)</b>	<b>6.943 02(+6)</b>
-6.8	<b>3.020 90(+5)</b>	<b>8.238 72(+5)</b>	<b>2.261 86(+6)</b>	<b>6.251 83(+6)</b>
-6.7	<b>2.761 97(+5)</b>	<b>7.490 04(+5)</b>	<b>2.045 12(+6)</b>	<b>5.623 09(+6)</b>
-6.6	<b>2.522 50(+5)</b>	<b>6.801 87(+5)</b>	<b>1.847 07(+6)</b>	<b>5.051 81(+6)</b>
-6.5	<b>2.301 26(+5)</b>	<b>6.169 96(+5)</b>	<b>1.666 29(+6)</b>	<b>4.533 29(+6)</b>
-6.4	<b>2.097 07(+5)</b>	<b>5.590 36(+5)</b>	<b>1.501 46(+6)</b>	<b>4.063 22(+6)</b>
-6.3	<b>1.908 82(+5)</b>	<b>5.059 32(+5)</b>	<b>1.351 33(+6)</b>	<b>3.637 54(+6)</b>
-6.2	<b>1.735 46(+5)</b>	<b>4.573 31(+5)</b>	<b>1.214 73(+6)</b>	<b>3.252 52(+6)</b>
-6.1	<b>1.575 97(+5)</b>	<b>4.129 03(+5)</b>	<b>1.090 67(+6)</b>	<b>2.904 70(+6)</b>
-6.0	<b>1.429 43(+5)</b>	<b>3.723 36(+5)</b>	<b>9.780 44(+5)</b>	<b>2.590 85(+6)</b>
-5.9	<b>1.294 92(+5)</b>	<b>3.353 39(+5)</b>	<b>8.759 54(+5)</b>	<b>2.308 01(+6)</b>
-5.8	<b>1.171 62(+5)</b>	<b>3.016 38(+5)</b>	<b>7.835 26(+5)</b>	<b>2.053 43(+6)</b>
-5.7	<b>1.058 72(+5)</b>	<b>2.709 78(+5)</b>	<b>6.999 51(+5)</b>	<b>1.824 58(+6)</b>
-5.6	<b>9.554 65(+4)</b>	<b>2.431 20(+5)</b>	<b>6.244 77(+5)</b>	<b>1.619 12(+6)</b>
-5.5	<b>8.611 59(+4)</b>	<b>2.178 39(+5)</b>	<b>5.564 08(+5)</b>	<b>1.434 90(+6)</b>
-5.4	<b>7.751 34(+4)</b>	<b>1.949 27(+5)</b>	<b>4.950 96(+5)</b>	<b>1.269 94(+6)</b>
-5.3	<b>6.967 64(+4)</b>	<b>1.741 90(+5)</b>	<b>4.399 46(+5)</b>	<b>1.122 43(+6)</b>
-5.2	<b>6.254 64(+4)</b>	<b>1.554 46(+5)</b>	<b>3.904 05(+5)</b>	<b>9.907 08(+5)</b>
-5.1	<b>5.606 83(+4)</b>	<b>1.385 27(+5)</b>	<b>3.459 64(+5)</b>	<b>8.732 35(+5)</b>
-5.0	<b>5.019 06(+4)</b>	<b>1.232 76(+5)</b>	<b>3.061 53(+5)</b>	<b>7.686 20(+5)</b>
-4.9	<b>4.486 52(+4)</b>	<b>1.095 49(+5)</b>	<b>2.705 40(+5)</b>	<b>6.755 87(+5)</b>
-4.8	<b>4.004 70(+4)</b>	<b>9.721 00(+4)</b>	<b>2.387 28(+5)</b>	<b>5.929 72(+5)</b>
-4.7	<b>3.569 41(+4)</b>	<b>8.613 58(+4)</b>	<b>2.103 53(+5)</b>	<b>5.197 14(+5)</b>
-4.6	<b>3.176 74(+4)</b>	<b>7.621 12(+4)</b>	<b>1.850 80(+5)</b>	<b>4.548 48(+5)</b>
-4.5	<b>2.823 03(+4)</b>	<b>6.733 00(+4)</b>	<b>1.626 05(+5)</b>	<b>3.974 98(+5)</b>
-4.4	<b>2.504 91(+4)</b>	<b>5.939 46(+4)</b>	<b>1.426 46(+5)</b>	<b>3.468 68(+5)</b>
-4.3	<b>2.219 25(+4)</b>	<b>5.231 51(+4)</b>	<b>1.249 50(+5)</b>	<b>3.022 39(+5)</b>
-4.2	<b>1.963 12(+4)</b>	<b>4.600 90(+4)</b>	<b>1.092 83(+5)</b>	<b>2.629 59(+5)</b>
-4.1	<b>1.733 84(+4)</b>	<b>4.040 07(+4)</b>	<b>9.543 58(+4)</b>	<b>2.284 38(+5)</b>
-4.0	<b>1.528 93(+4)</b>	<b>3.542 08(+4)</b>	<b>8.321 49(+4)</b>	<b>1.981 49(+5)</b>
-3.9	<b>1.346 09(+4)</b>	<b>3.100 61(+4)</b>	<b>7.244 67(+4)</b>	<b>1.716 14(+5)</b>
-3.8	<b>1.183 21(+4)</b>	<b>2.709 86(+4)</b>	<b>6.297 36(+4)</b>	<b>1.484 04(+5)</b>
-3.7	<b>1.038 36(+4)</b>	<b>2.364 59(+4)</b>	<b>5.465 34(+4)</b>	<b>1.281 35(+5)</b>
-3.6	<b>9.097 56(+3)</b>	<b>2.060 00(+4)</b>	<b>4.735 76(+4)</b>	<b>1.104 62(+5)</b>
-3.5	<b>7.957 69(+3)</b>	<b>1.791 74(+4)</b>	<b>4.097 06(+4)</b>	<b>9.507 83(+4)</b>
-3.4	<b>6.949 11(+3)</b>	<b>1.555 89(+4)</b>	<b>3.538 83(+4)</b>	<b>8.170 81(+4)</b>
-3.3	<b>6.058 24(+3)</b>	<b>1.348 87(+4)</b>	<b>3.051 75(+4)</b>	<b>7.010 72(+4)</b>
-3.2	<b>5.272 73(+3)</b>	<b>1.167 47(+4)</b>	<b>2.627 46(+4)</b>	<b>6.005 80(+4)</b>
-3.1	<b>4.581 32(+3)</b>	<b>1.008 79(+4)</b>	<b>2.258 49(+4)</b>	<b>5.136 72(+4)</b>
-3.0	<b>3.973 81(+3)</b>	<b>8.702 36(+3)</b>	<b>1.938 16(+4)</b>	<b>4.386 36(+4)</b>
-2.9	<b>3.440 99(+3)</b>	<b>7.494 54(+3)</b>	<b>1.660 55(+4)</b>	<b>3.739 60(+4)</b>

Table 3d (continued)

$x$	$I_{13/2}(x)$	$I_7(x)$	$I_{15/2}(x)$	$I_8(x)$
-2.8	<b>2.97449(+3)</b>	<b>6.44353(+3)</b>	<b>1.42036(+4)</b>	<b>3.18306(+4)</b>
-2.7	<b>2.56681(+3)</b>	<b>5.53057(+3)</b>	<b>1.21290(+4)</b>	<b>2.70496(+4)</b>
-2.6	<b>2.21118(+3)</b>	<b>4.73894(+3)</b>	<b>1.03404(+4)</b>	<b>2.29493(+4)</b>
-2.5	<b>1.90151(+3)</b>	<b>4.05373(+3)</b>	<b>8.80080(+3)</b>	<b>1.94389(+4)</b>
-2.4	<b>1.63236(+3)</b>	<b>3.46168(+3)</b>	<b>7.47797(+3)</b>	<b>1.64385(+4)</b>
-2.3	<b>1.39885(+3)</b>	<b>2.95154(+3)</b>	<b>6.34335(+3)</b>	<b>1.38785(+4)</b>
-2.2	<b>1.19665(+3)</b>	<b>2.51139(+3)</b>	<b>5.37187(+3)</b>	<b>1.16979(+4)</b>
-2.1	<b>1.02187(+3)</b>	<b>2.13342(+3)</b>	<b>4.54153(+3)</b>	<b>9.84373(+3)</b>
-2.0	<b>8.71082(+2)</b>	<b>1.80956(+3)</b>	<b>3.83307(+3)</b>	<b>8.26978(+3)</b>
-1.9	<b>7.41232(+2)</b>	<b>1.53205(+3)</b>	<b>3.22968(+3)</b>	<b>6.93603(+3)</b>
-1.8	<b>6.29622(+2)</b>	<b>1.29486(+3)</b>	<b>2.71667(+3)</b>	<b>5.80776(+3)</b>
-1.7	<b>5.33869(+2)</b>	<b>1.09250(+3)</b>	<b>2.28128(+3)</b>	<b>4.85497(+3)</b>
-1.6	<b>4.51876(+2)</b>	<b>9.20164(+2)</b>	<b>1.91243(+3)</b>	<b>4.05176(+3)</b>
-1.5	<b>3.81793(+2)</b>	<b>7.73670(+2)</b>	<b>1.60049(+3)</b>	<b>3.37582(+3)</b>
-1.4	<b>3.22007(+2)</b>	<b>6.49368(+2)</b>	<b>1.23717(+3)</b>	<b>2.80797(+3)</b>
-1.3	<b>2.71099(+2)</b>	<b>5.44091(+2)</b>	<b>1.11527(+3)</b>	<b>2.33176(+3)</b>
-1.2	<b>2.27832(+2)</b>	<b>4.55089(+2)</b>	<b>9.28610(+2)</b>	<b>1.93309(+3)</b>
-1.1	<b>1.91130(+2)</b>	<b>3.79983(+2)</b>	<b>7.71879(+2)</b>	<b>1.59992(+3)</b>
-1.0	<b>1.60054(+2)</b>	<b>3.16721(+2)</b>	<b>6.40510(+2)</b>	<b>1.32196(+3)</b>
-0.9	<b>1.33792(+2)</b>	<b>2.63532(+2)</b>	<b>5.30595(+2)</b>	<b>1.09049(+3)</b>
-0.8	<b>1.11640(+2)</b>	<b>2.18894(+2)</b>	<b>4.38795(+2)</b>	<b>8.98032(+2)</b>
-0.7	<b>9.29891(+1)</b>	<b>1.81500(+2)</b>	<b>3.62261(+2)</b>	<b>7.38318(+2)</b>
-0.6	<b>7.73164(+1)</b>	<b>1.50233(+2)</b>	<b>2.98568(+2)</b>	<b>6.05999(+2)</b>
-0.5	<b>6.41709(+1)</b>	<b>1.24137(+2)</b>	<b>2.45655(+2)</b>	<b>4.96567(+2)</b>
-0.4	<b>5.31657(+1)</b>	<b>1.02395(+2)</b>	<b>2.01777(+2)</b>	<b>4.06220(+2)</b>
-0.3	<b>4.39696(+1)</b>	<b>8.43150(+1)</b>	<b>1.65455(+2)</b>	<b>3.31759(+2)</b>
-0.2	<b>3.62996(+1)</b>	<b>6.93070(+1)</b>	<b>1.35441(+2)</b>	<b>2.70497(+2)</b>
-0.1	<b>2.99145(+1)</b>	<b>5.68718(+1)</b>	<b>1.10684(+2)</b>	<b>2.20182(+2)</b>
0.0	<b>2.46088(+1)</b>	<b>4.65871(+1)</b>	<b>9.02998(+1)</b>	<b>1.78930(+2)</b>
0.1	<b>2.02084(+1)</b>	<b>3.80963(+1)</b>	<b>7.35450(+1)</b>	<b>1.45165(+2)</b>
0.2	<b>1.65656(+1)</b>	<b>3.10994(+1)</b>	<b>5.97980(+1)</b>	<b>1.17578(+2)</b>
0.3	<b>1.35555(+1)</b>	<b>2.53438(+1)</b>	<b>4.85386(+1)</b>	<b>9.50756(+1)</b>
0.4	<b>1.10729(+1)</b>	<b>2.06179(+1)</b>	<b>3.93330(+1)</b>	<b>7.67533(+1)</b>
0.5	<b>9.02903(0)</b>	<b>1.67445(+1)</b>	<b>3.18197(+1)</b>	<b>6.18599(+1)</b>
0.6	<b>7.34955(0)</b>	<b>1.35755(+1)</b>	<b>2.56985(+1)</b>	<b>4.97744(+1)</b>
0.7	<b>5.97201(0)</b>	<b>1.09874(+1)</b>	<b>2.07200(+1)</b>	<b>3.99844(+1)</b>
0.8	<b>4.84419(0)</b>	<b>8.87753(0)</b>	<b>1.66781(+1)</b>	<b>3.20673(+1)</b>
0.9	<b>3.92253(0)</b>	<b>7.16060(0)</b>	<b>1.34022(+1)</b>	<b>2.56757(+1)</b>
1.0	<b>3.17070(0)</b>	<b>5.76592(0)</b>	<b>1.07519(+1)</b>	<b>2.05245(+1)</b>
1.1	<b>2.55853(0)</b>	<b>4.63500(0)</b>	<b>8.61132(0)</b>	<b>1.63800(+1)</b>
1.2	<b>2.06099(0)</b>	<b>3.71959(0)</b>	<b>6.88547(0)</b>	<b>1.30511(+1)</b>
1.3	<b>1.65734(0)</b>	<b>2.97994(0)</b>	<b>5.49639(0)</b>	<b>1.03818(+1)</b>
1.4	<b>1.33045(0)</b>	<b>2.38334(0)</b>	<b>4.38029(0)</b>	<b>8.24509(0)</b>
1.5	<b>1.06620(0)</b>	<b>1.90298(0)</b>	<b>3.48508(0)</b>	<b>6.53752(0)</b>
1.6	<b>8.52973(-1)</b>	<b>1.51689(0)</b>	<b>2.76826(0)</b>	<b>5.17521(0)</b>
1.7	<b>6.81225(-1)</b>	<b>1.20711(0)</b>	<b>2.19526(0)</b>	<b>4.09017(0)</b>
1.8	<b>5.43131(-1)</b>	<b>9.58990(-1)</b>	<b>1.73802(0)</b>	<b>3.22742(0)</b>
1.9	<b>4.32296(-1)</b>	<b>7.60600(-1)</b>	<b>1.37376(0)</b>	<b>2.54255(0)</b>
2.0	<b>3.43496(-1)</b>	<b>6.02251(-1)</b>	<b>1.08407(0)</b>	<b>1.99980(0)</b>

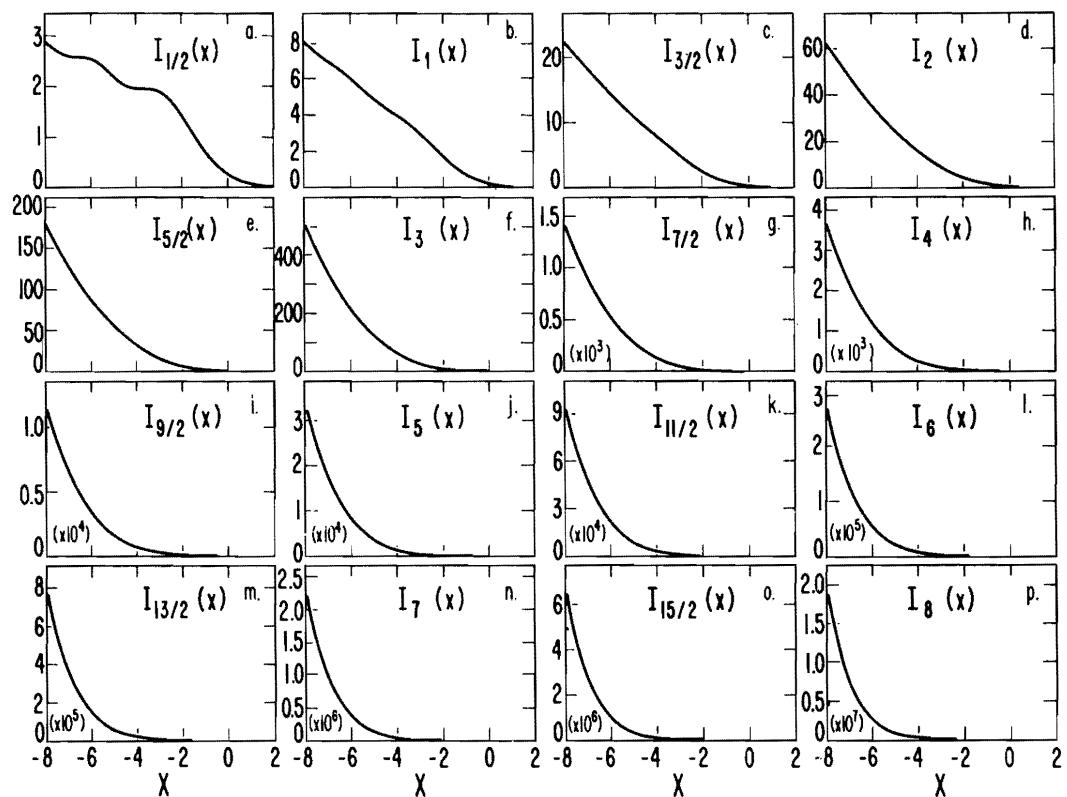


Figure 7. The Integrals  $I_v(x) = \int_x^\infty (y-x)^v \text{Ai}(y) dy$  for  $x \in [-7.9, 2]$  and  $v = 1/2, 1, 3/2, \dots, 8$

A similar table has been published recently [14] using an interpolative technique for generating the Airy function. The numbers presented in Table 3 were generated independently of those in Reference [14] and are included here for completeness.

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